

Improving Wastewater Oxygenation & Mixing Efficiency with Solar Powered Circulation

H. Kenneth Hudnell, PhD

- **SolarBee, Inc., VP & Director of Science**
- **The University of North Carolina at Chapel Hill - Institute for the Environment, Adjunct Associate Research Professor**
- **US Environmental Protection Agency, Neurotoxicologist, 1984-2007**

Contact Information: **Phone - 919-932-7229**
 Email - kenhud@SolarBee.com

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Co-Authors

David Green, Publics Works Department, City of Rochester, Rochester, NH, USA

Ron Vein, Pittsfield Water Department, Pittsfield, NH, USA

Scott Butler, Water and Sewer Division, Town of Exeter, Exeter, NH, USA

Greg Rahe, Engineering Dept., Public Service of New Hampshire, Manchester, NH

Bruce Richards, SolarBee, Inc., Newark, DE, USA

Joel Bleth, SolarBee Headquarters, 3225 Highway 22, Dickinson, ND, 58601, USA

Overview

- The problem - mixing with aeration is inefficient
- U.S. EPA preliminary data
- The current study
 - The NHDES directed a 3 site study on Solar Powered Circulation (SPC) to reduce or eliminate the need for aeration to mix & oxygenate wastewater
 - Data collected 1 year pre-SPC & 2 years during-SPC
 - Effluent water quality, odor events, sludge buildup
- ◆ No pre- versus during-SPC water quality differences
- ◆ 37.5-88.5% drop in power use; 1.9-3.7 year payback

Journal submission:

A paper using these data and entitled, *Improving Wastewater Mixing and Oxygenation Efficiency with Solar Powered Circulation (SPC)*, will be submitted for peer review to the journal, *Clean Technology & Environmental Policy*, immediately after this meeting

The Problem

- Most wastewater treatment plants require mixing & oxygenation to increase organic-matter digestion rates
- WWTPs typically use grid-powered mechanical aerators to both mix & oxygenate the wastewater
- Mixing usually requires much more aeration than oxygenation
- This imbalance creates an operational inefficiency
 - Excessive grid-power consumption & expenditure
 - Increased greenhouse gas emissions

Preliminary Data



Auxiliary and Supplemental Power Fact Sheet: Solar Power

EPA 832-F-05-011, Office of Water, March 2005, Revised October 2007



- Reviewed information from 4 WWTPs using SPC
- Concluded benefits include energy savings, & reduced odor, greenhouse gas emissions & biosolids

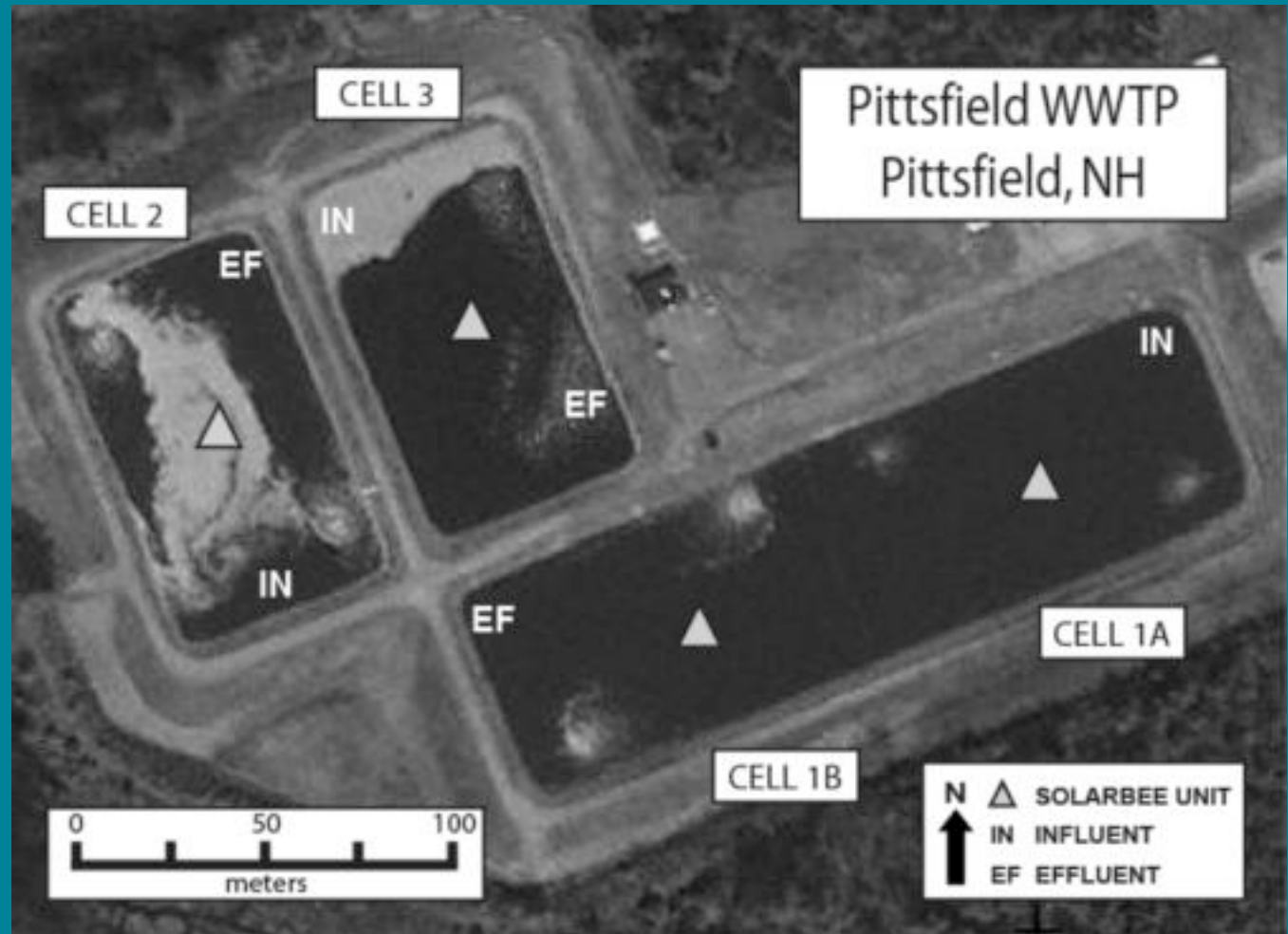
Current Study

- **Directed by the New Hampshire Department of Public Services**
- **Goal - Increase operational efficiency (reduce cost)**
- **Objectives**
 - **Reduce or eliminate grid-powered aeration**
 - **Maintain or improve effluent water quality**
- **Data collected by personnel at 3 NH WWTPs 1 year before and 2 years during SPC**
 - **Flow rate, total suspended solids (TSS), biochemical oxygen demand (BOD), ammonia, nitrate, odor, sludge**
 - **Electric grid power consumption & expenditures**

Study Sites - Pittsfield, NH

Pre-SPC

Lagoons with
65 kW
fine bubble
blower
system



Secondary treatment plant using aerated lagoons

Study Sites - Rochester, NH

Pre-SPC

Lagoons with
116 kW
fine bubble
blower
system



During-SPC

Converted to
equalization
basins also
receiving
sludge, raw
septage,
backwash &
raw sewage

Activated sludge, advanced tertiary-treatment plant

Table 1. Location, Cell & Treatment Parameters

	Exeter			Pittsfield				Rochester	
	Cell 1	Cell 2	Cell 3	Cell 1a	Cell 1b	Cell 2	Cell 3	Cell 1	Cell 2
Surface Area (km ²)	0.036	0.034	0.034	0.0054	0.0054	0.0053	0.0053	0.046	0.028
Operating Depth (m)	2.59	2.59	2.59	3.35	3.35	3.35	3.35	2.13	2.13
Operating Volume (km ³)	6.19x10 ⁻⁵	5.87x10 ⁻⁵	5.12x10 ⁻⁵	1.17x10 ⁻⁵	1.17x10 ⁻⁵	1.16x10 ⁻⁵	1.16x10 ⁻⁵	6.86x10 ⁻⁷	4.17x10 ⁻⁷
Influent Depth (m) ^a	1.22	V ^a	V ^a	3.25	3.25	3.25	3.25	1.52	1.52
Effluent Depth (m) ^a	1.52	1.2	1.2	3.00	3.00	3.00	3.00	V ^a	V ^a
Discharge Method ^a	C	C	C	C	C	C	C	C/I ^c	C/I ^c
Detention Time (days)	8.2	7.8	6.8	6.16	6.16	6.12	6.12	47	47
# SPC Units	2	2	2	1	1	1 ^d	1 ^d	3	2
Surface Area km ² /SPC unit	0.018	0.017	0.017	0.0054	0.0054	0.0053	0.0053	0.015	0.014
Mean Intake Depth (m)	1.37	1.52	1.52	1.21	1.12	0.76	1.5	0.61	0.61
Water Volume Circulated (km ³)	3.27x10 ⁻⁵	3.44x10 ⁻⁵	3.00x10 ⁻⁵	4.23x10 ⁻⁶	3.91x10 ⁻⁶	2.65x10 ⁻⁶	5.19x10 ⁻⁶	3.23x10 ⁻⁷	4.18x10 ⁻⁸
Water km ³ Circulated/SPC unit (km ³)	1.64x10 ⁻⁵	1.72x10 ⁻⁵	1.50x10 ⁻⁵	4.23x10 ⁻⁶	3.91x10 ⁻⁶	2.65x10 ⁻⁶	5.19x10 ⁻⁶	1.39x10 ⁻⁸	2.08x10 ⁻⁸
SPC Circulation Rate (km ³ /day)	5.5x10 ⁻⁵	5.5x10 ⁻⁵	5.5x10 ⁻⁵	5.5x10 ⁻⁵	5.5x10 ⁻⁵	1.36x10 ⁻⁵	1.36x10 ⁻⁵	5.5x10 ⁻⁵	5.5x10 ⁻⁵
Total Circulation Rate (km ³ /day)	1.1x10 ⁻⁴	1.1x10 ⁻⁴	1.1x10 ⁻⁴	5.5x10 ⁻⁵	5.5x10 ⁻⁵	1.36x10 ⁻⁵	1.36x10 ⁻⁵	1.65x10 ⁻⁴	1.1x10 ⁻⁴
Turnover Duration (days) ^e	0.30	0.31	0.27	0.08	0.07	0.19	0.38	0.003	0.0004

C=Continuous, I=Intermittent, NA=Not Available, V=Variable

^a Weir gate – 0.61-3.0 m from bottom

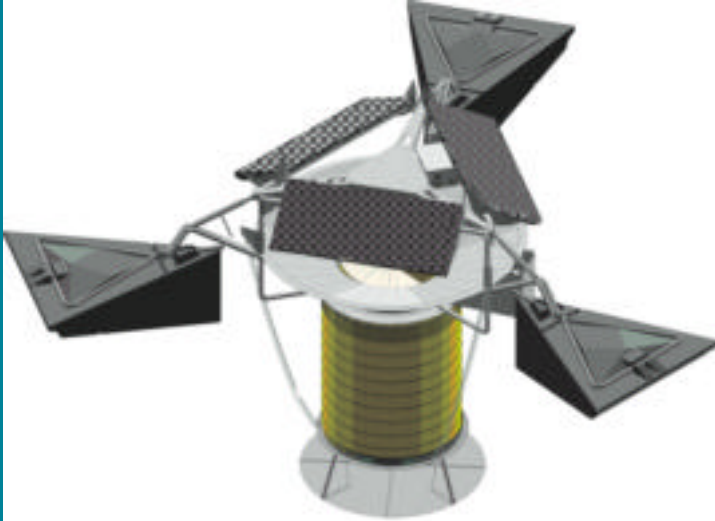
^b 3 sluice gate – top 0.61-1.52 m, middle 1.52-2.44 m, bottom 2.44-3.52 m from surface

^c Spring & fall continuous at 3,271 m³/d, Winter & summer intermittent at mean 818 m³/d

^d All SPC units were SB10000 models except SB2500 models indicated by a superscript d

^e The duration required for the SPC units to circulate all the water between the surface and mean intake depth one time

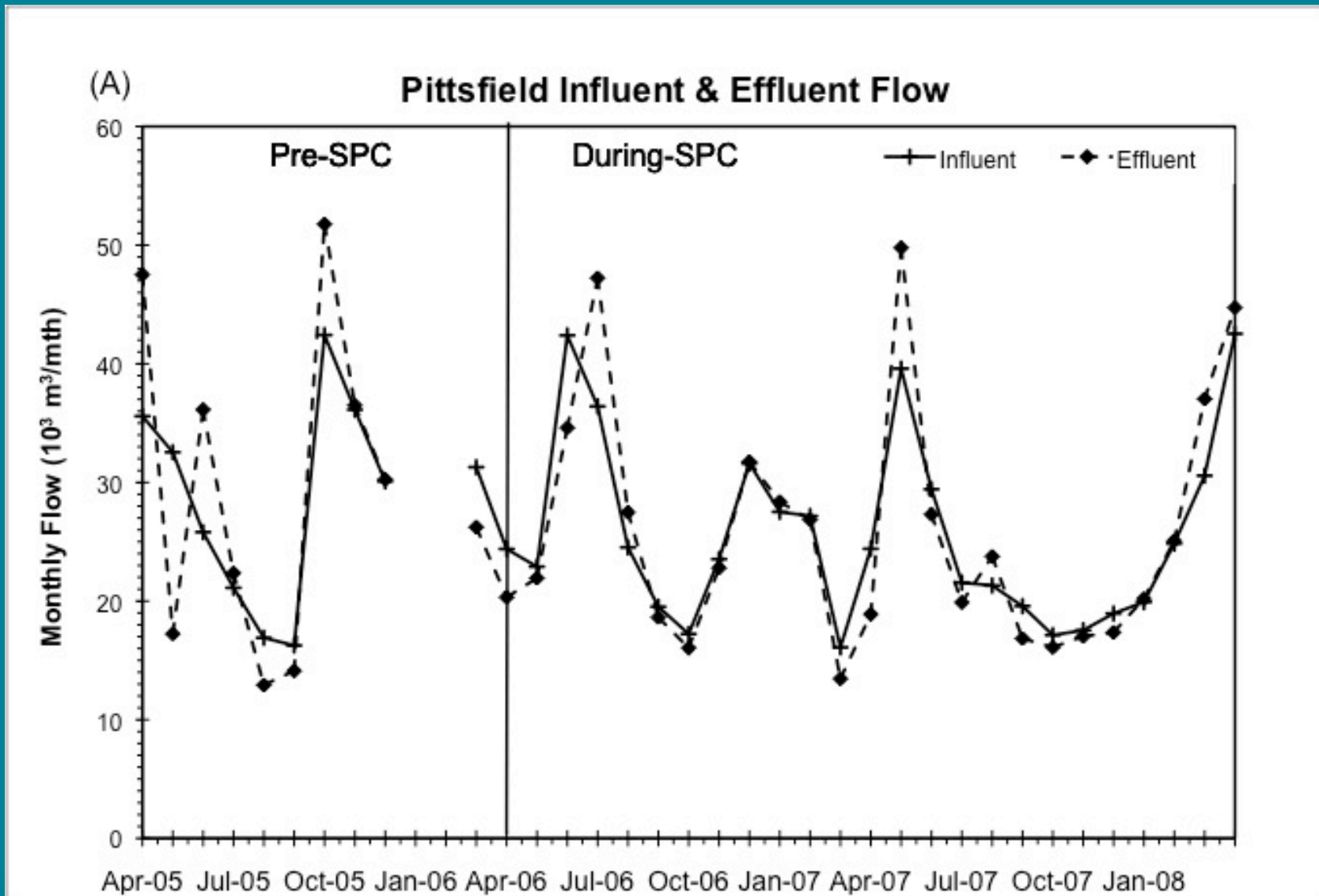
Solar Powered Circulation



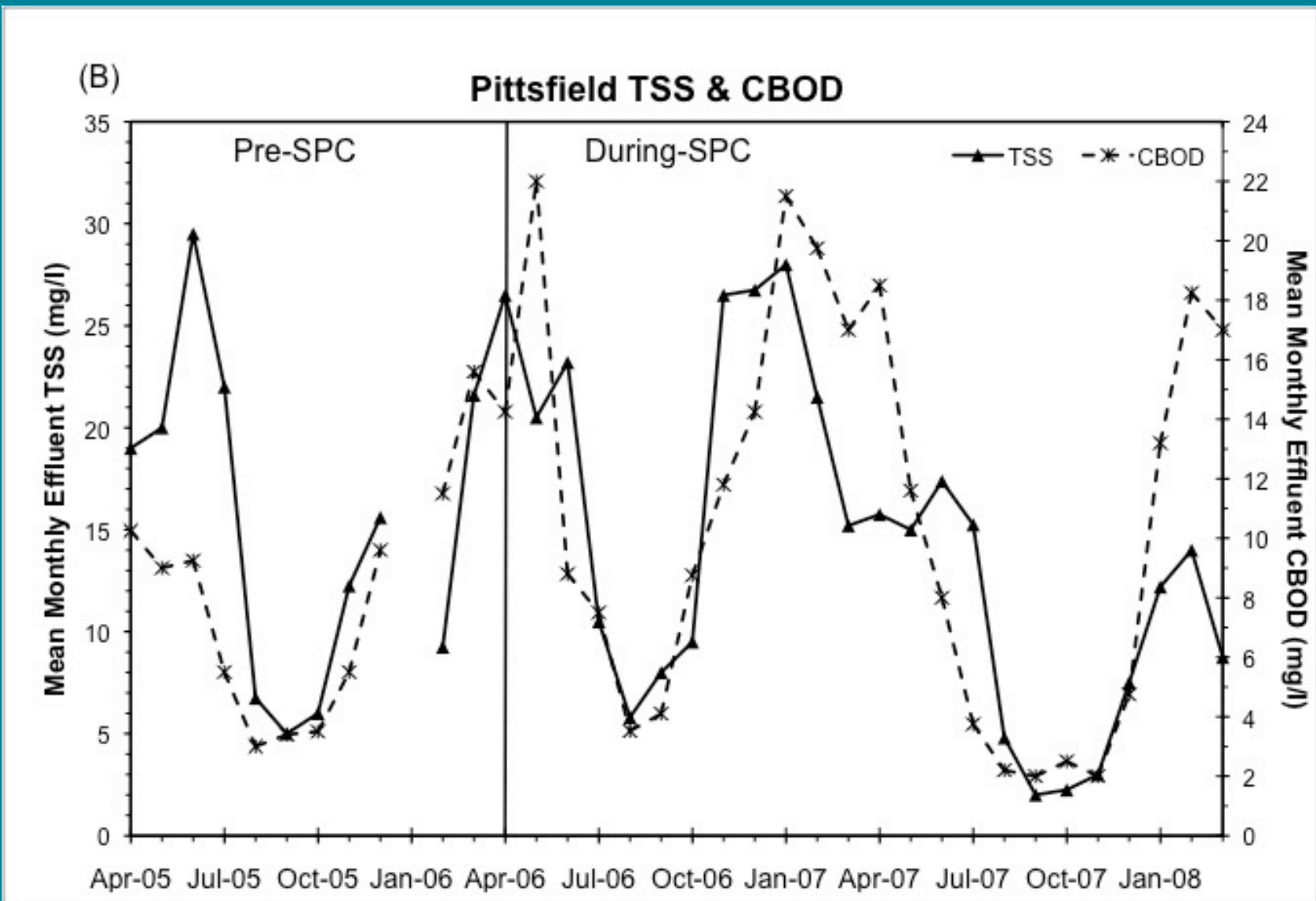
Pittsfield site

- 316 Stainless steel construction
- Three foam filled HDPE pontoons
- Two HDPE coated concrete mooring blocks
- Three 80 watt solar panels
- 18 Volt direct-drive motor & battery
- Continuous day/night operation at 80 RPM
- 3 ft diameter thermoplastic rubber intake hose, length adjustable
- Stainless plate suspended 1 ft below hose intake
- Near-laminar radial inflow
- 10,000 GPM upflow
- Non-turbulent outflow at surface

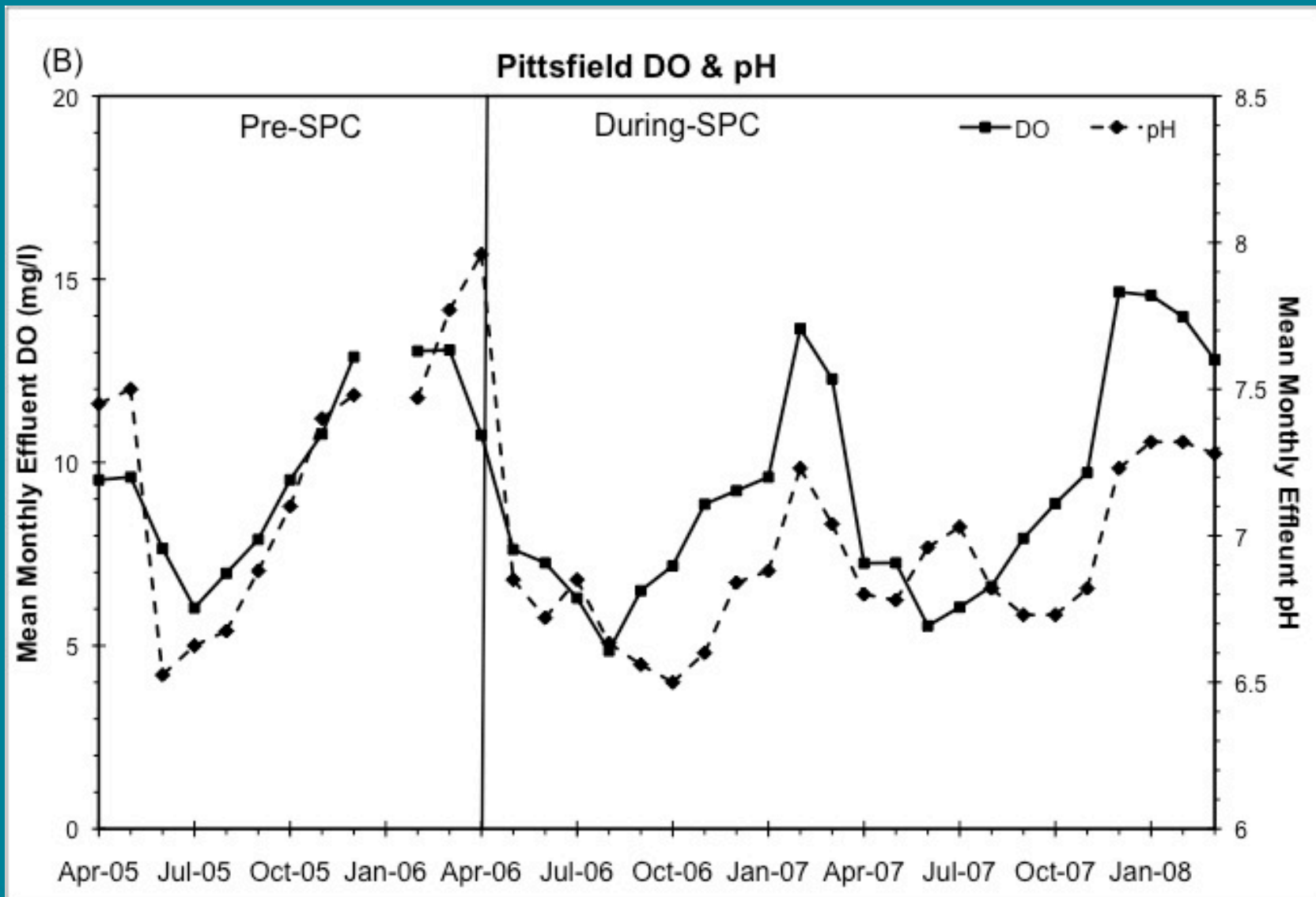
Pittsfield - Flow Rate



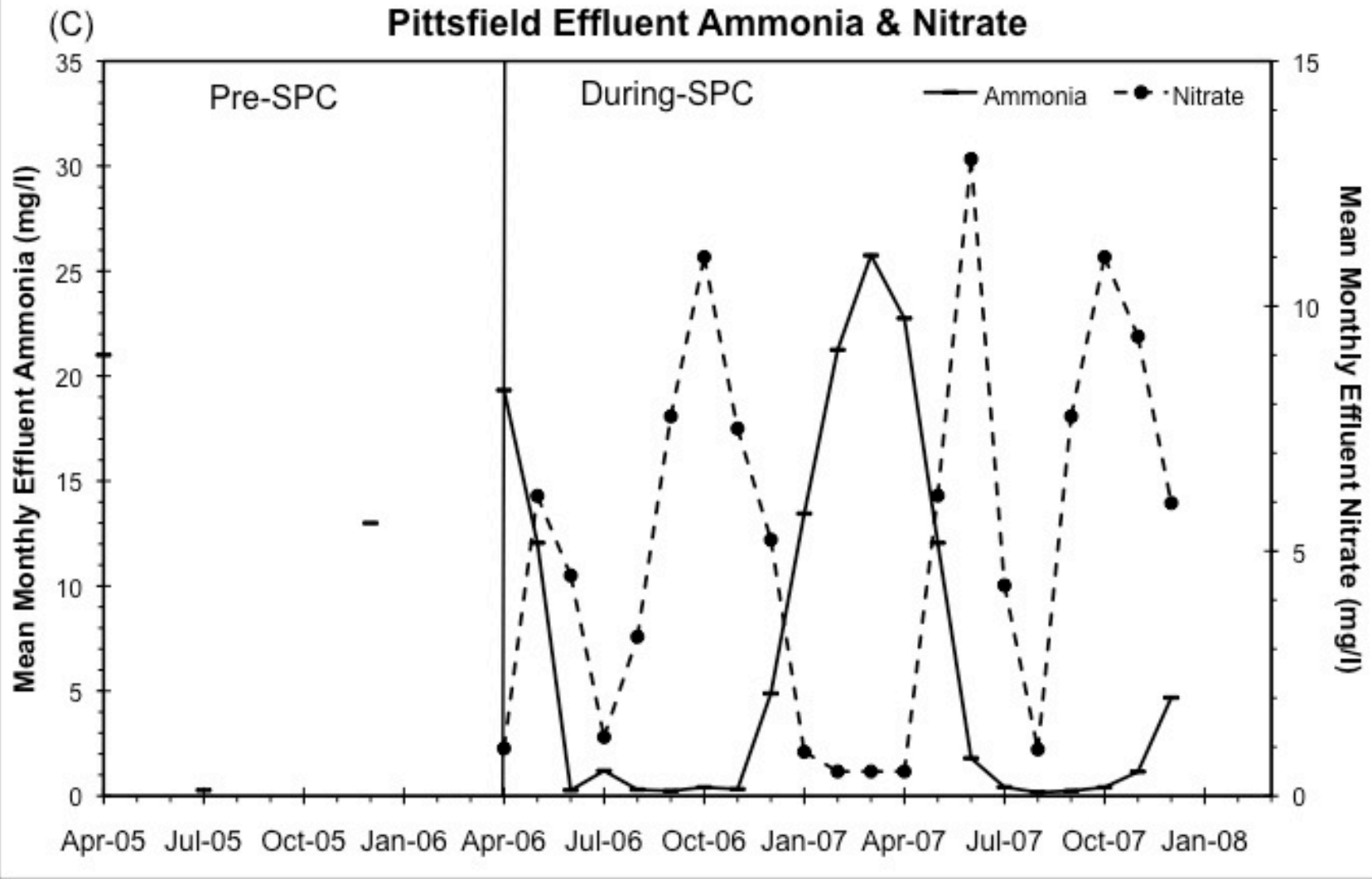
Pittsfield - TSS & CBOD



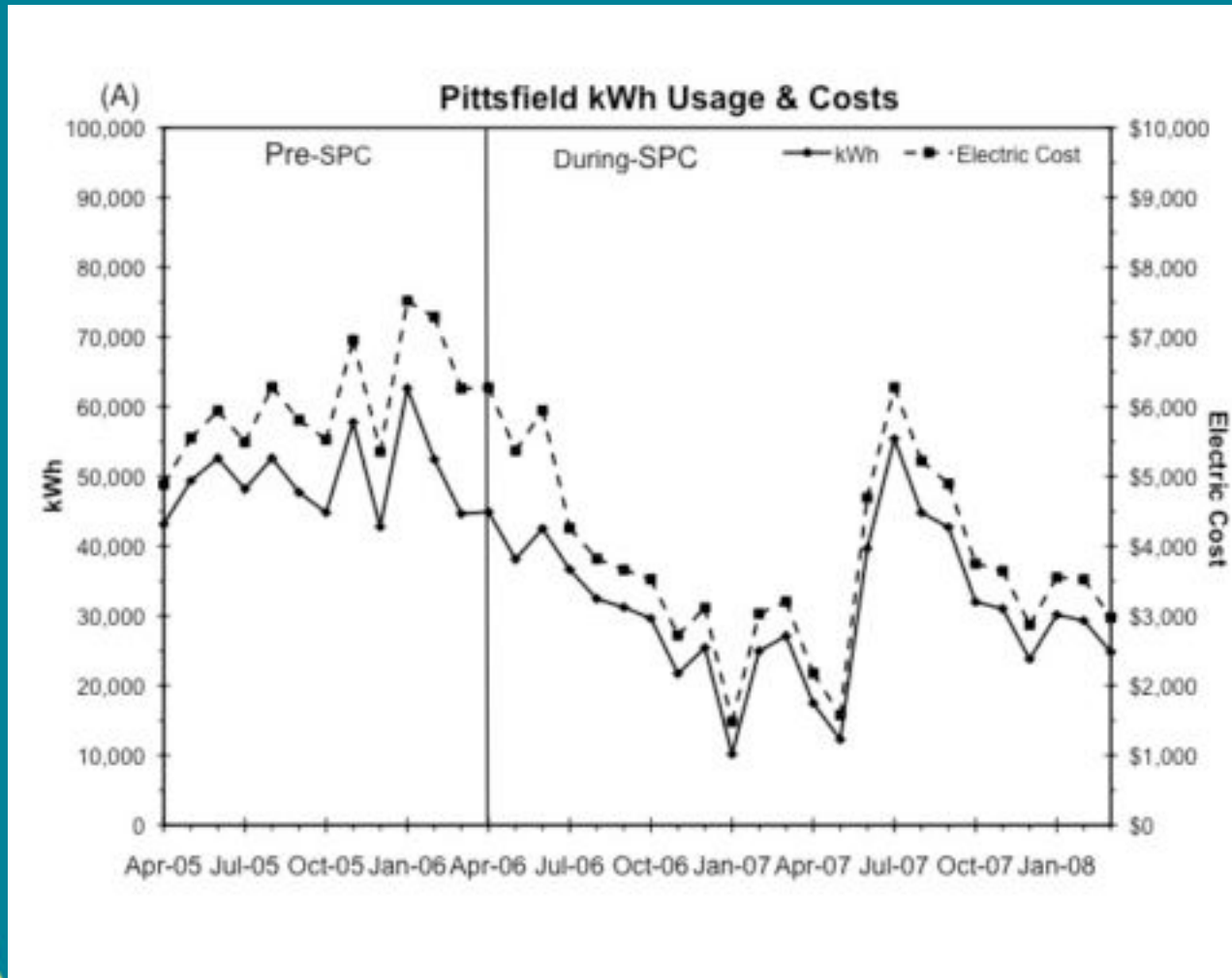
Pittsfield - DO & pH



Pittsfield - Ammonia & Nitrate



Pittsfield - kWh Usage & Cost



Reductions during SPC

kWh = 18,712/mth
= 224,540/yr
= 37.5%

Cost = \$2,256/mth
= \$27,068/yr
= 37.2%

Pay back period
= 3.7 yrs

All 3 Sites

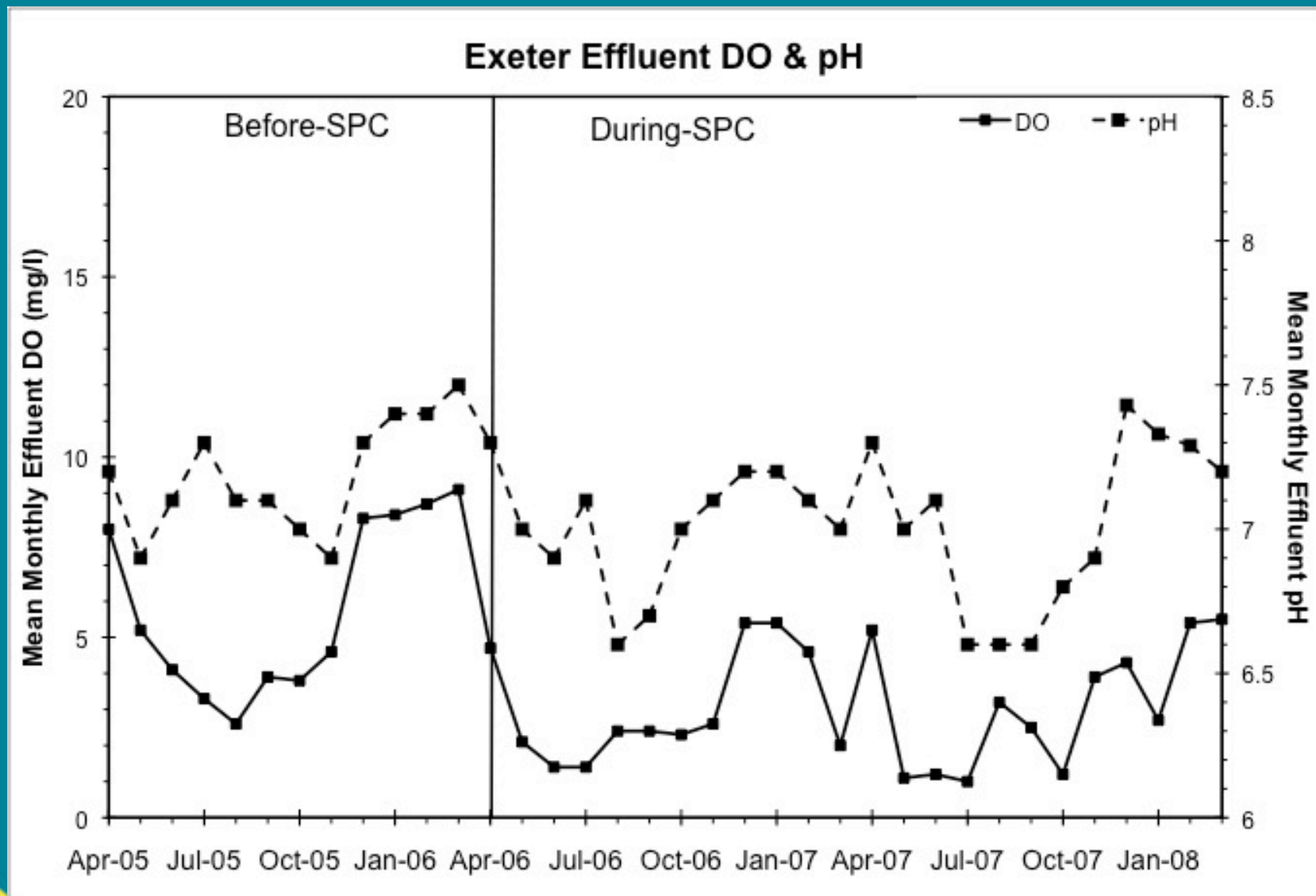
- No NPDES violations occurred during SPC
- No odor events during SPC
 - Maintaining 1-2 mg/l DO in the top 0.5-1 m oxidized toxic hydrogen sulfide to odorless sulfate
- Little or no sludge accumulation during 2 years of SPC
 - CO₂, acids, alcohols & then CH₄ are formed & emitted to air during sludge digestion. SPC stimulates green algae that consume CO₂ during photosynthesis, increasing pH and improving the function of CH₄ forming anaerobic bacteria in the sludge & slurry.
 - SPC eliminated the neuston layer of lipids & proteins, increasing CH₄ & CO₂ emissions

Exeter Results

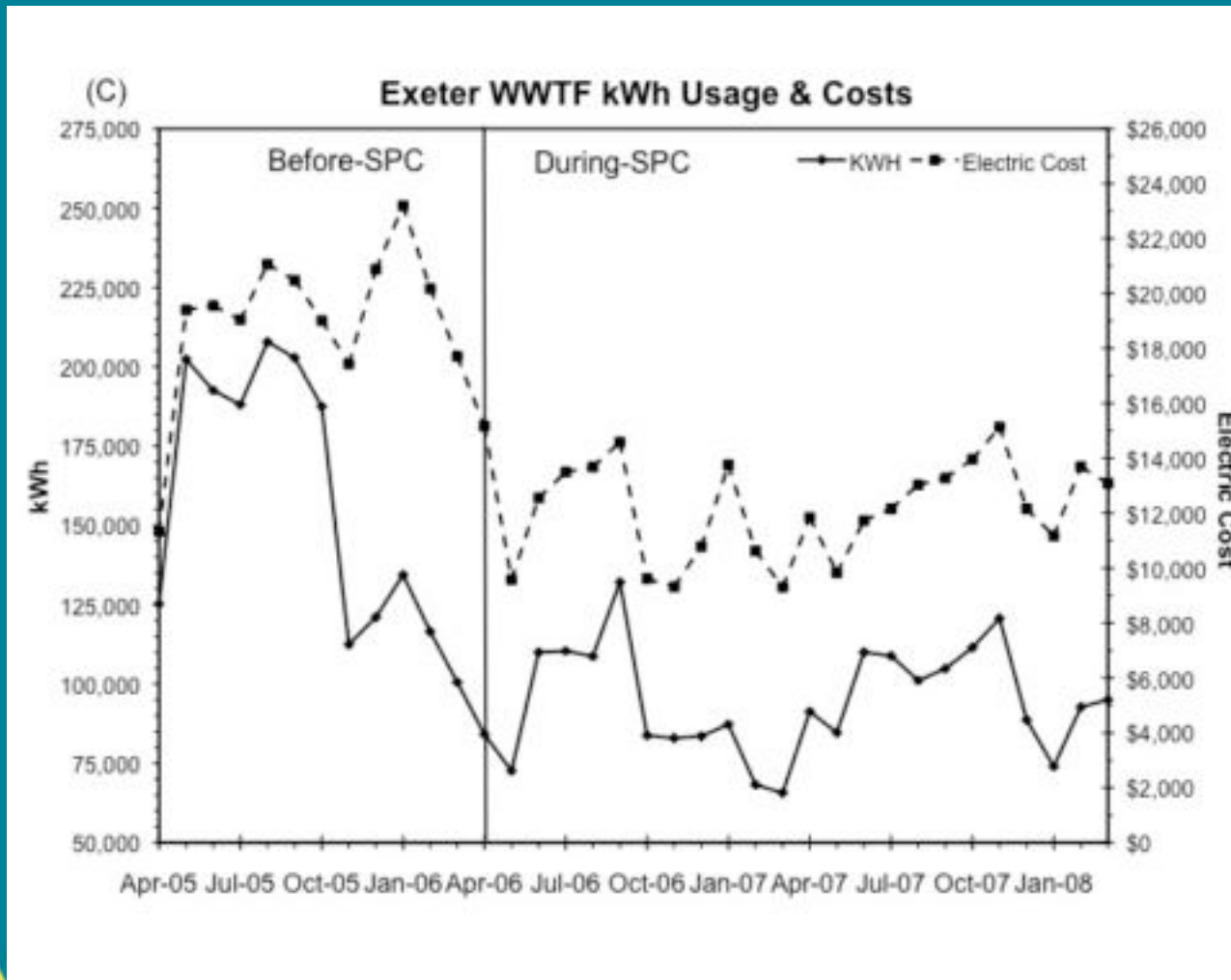
➤ No statistically significant differences between Pre-SPC & During-SPC study periods in the following parameters (During-SPC mean values shown)

- Effluent flow rate ($60.6_{\pm}21.2 \times 10^3 \text{ m}^3/\text{mth}$)
- TSS (12.7_{\pm} mg/l)
- BOD ($12.0_{\pm}4.7 \text{ mg/l}$)
- pH ($7.2_{\pm}0.2 \text{ su}$)
- Ammonia ($9.9_{\pm}4.9 \text{ mg/l}$)
- Nitrate not measured

Exeter DO



Exeter - kWh Usage & Cost



Reductions during SPC

kWh = 62,896/mth
= 754,753/yr
= 40.0%

Cost = \$6,876/mth
= \$82,513/yr
= 36.0%

Pay back period
= 2.9 yrs

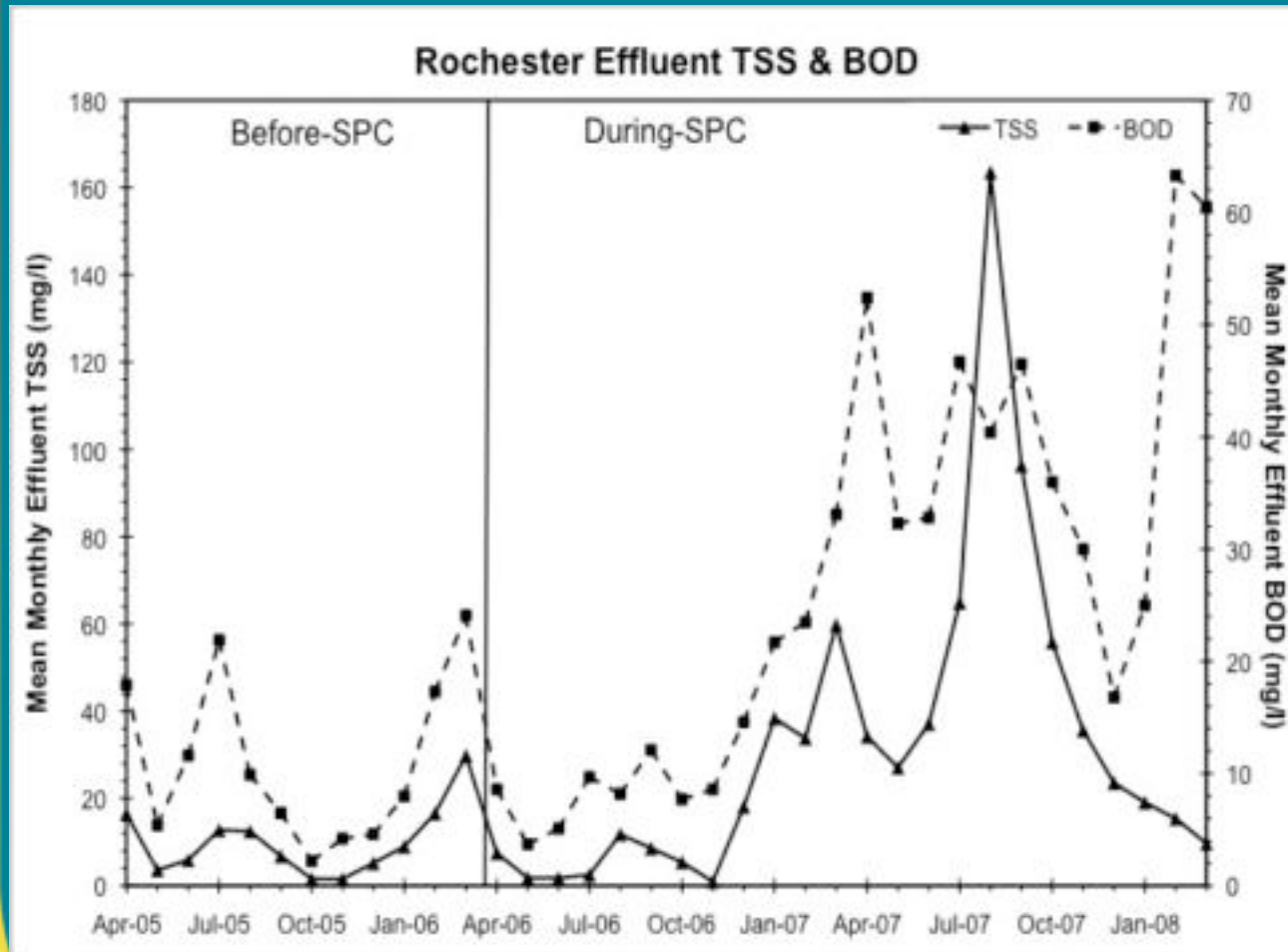
Rochester Results

➤ No statistically significant differences between Pre-SPC & During-SPC study periods in the following parameters (During-SPC values shown)

❖ Aerated lagoons converted to equalization basins

- Effluent flow rate ($712.1_{\pm}294.2$ m³/mth)
- DO ($4.3_{\pm}2.4$ mg/l)
- pH ($7.5_{\pm}0.2$ su)
- Ammonia ($16.7_{\pm}8.8$ mg/l)
- Nitrate not measured

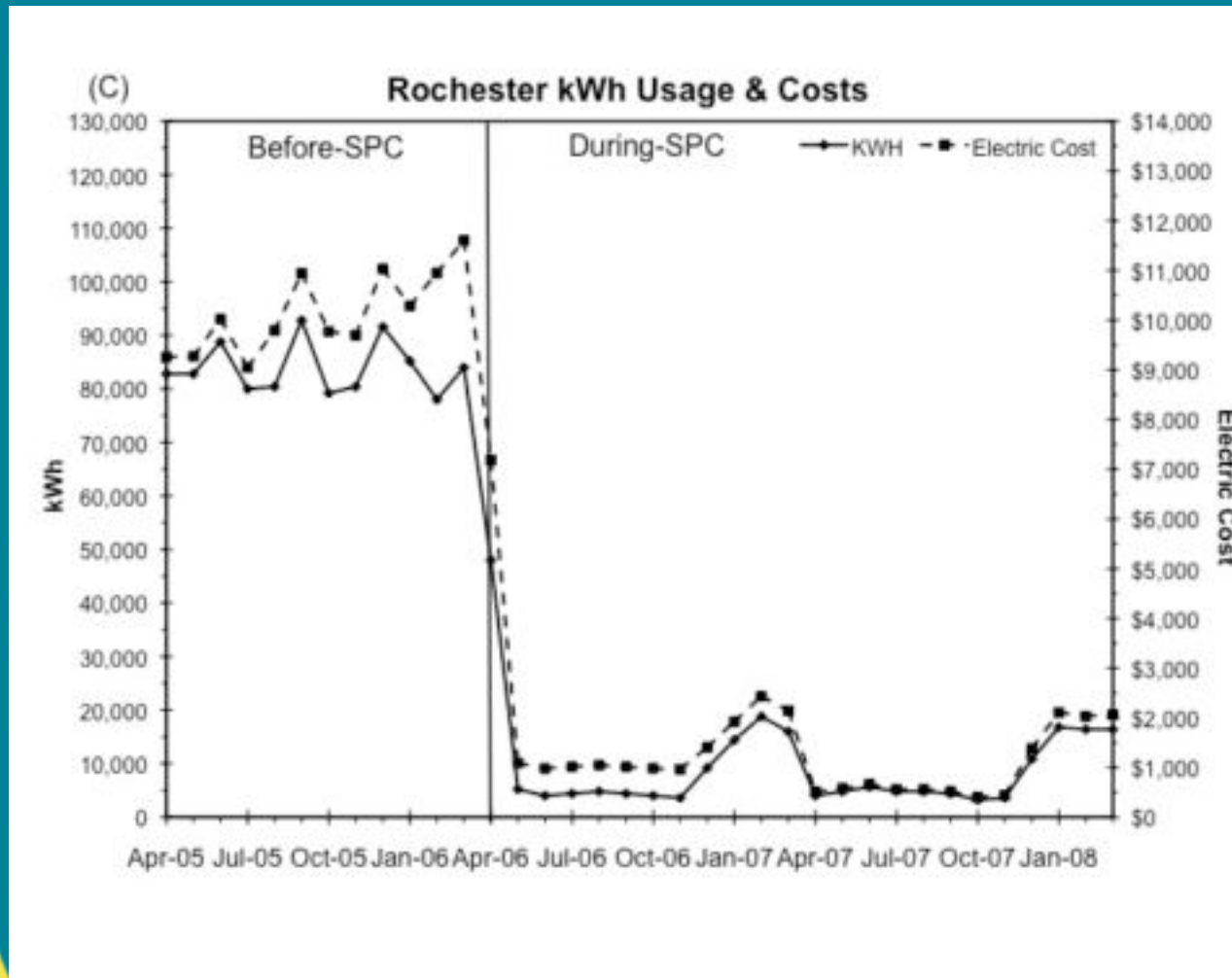
Rochester TSS & BOD



TSS & BOD increased significantly during SPC due to the conversion from aerated lagoons to equalization basins

Cell 2 reductions in TSS & BOD ranged from 30-40% before effluent transferred to anaerobic cells

Rochester - kWh Usage & Cost



Reductions during SPC

kWh = 74,150/mth
= 889,803/yr
= 88.5%

Cost = \$8,722/mth
= \$104,658/yr
= 86%

Pay back period
= 1.9 yrs

Conclusions

- Operational efficiency was increased by replacing some or all electrical grid-powered aeration at 3 WWTPs with SPC
- Effluent water quality was maintained, odor events were avoided, & sludge buildup was minimized
- Electrical grid-power consumption decreased by 37.5-88.5%
- Electrical grid-power expenditure decreased by 36-86%
- Payback periods ranged from 1.9-3.7 years
 - ◆ Long term operating expense reductions indicated by 25 yr unit lifetime & low maintenance needs

Thank You!

I'm happy to take any questions